

**Assessment of the Environmental Risks
Associated with the Use of Treated Wood
in Lotic Systems**

**This addendum is applicable to the Columbia River and other flowing waters where
Threatened or Endangered Species are Found. It includes recommendations for minimum
environmental parameters to protect sensitive aquatic species.**

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Assessment of the Environmental Risks Associated with the Use of Treated Wood in Lotic Systems

Introduction. This addendum is applicable to the Columbia River and other flowing waters where Threatened or Endangered Species are Found. It includes recommendations for minimum environmental parameters to protect sensitive aquatic species. Brooks (1995a, 1995b, 1995c) has produced a series of treated wood risk assessments supported by Microsoft EXCEL spreadsheet models. Dilution factors in these models were optimized for marine environments where harmonically driven tidal currents interact with steady state currents. In this paper, the models are modified to optimize their predictive capability in lotic systems with reasonably constant, unidirectional flow. In addition, this paper includes a discussion of metal and PAH stress in anadromous salmonids. This paper is an addendum to Brooks (1995a, 1995b, 1995c) and the reader is referred to these documents for a more detailed account of the underlying analysis.

The following model is conservative from the environments point of view. Laminar flows with no turbulent mixing are assumed and water column concentrations are predicted in the near field - within a few centimeters of the piling. The model assumes that PAH and copper are adsorbed to relatively large and dense particles (silt) which is deposited in close proximity to the piling or bulkhead. In reality, adsorption will be to a spectrum of particle sizes including clays and particulate organic matter with much slower settling rates. This will result in lower than predicted sediment concentrations.

Background levels of copper and PAH in the Columbia River. The current analysis integrates background levels of copper observed by Johnson and Hopkins (1991) in Columbia River water. The data in Table 1 is extracted from their report.

Table 1. Columbia River flows, hardness and copper concentrations. Total (unfiltered) copper is reported.

Parameter	Date			
	January 9	May 30	September 25	Average
Flow (CFS)	139,000	253,000	126,000	172,670 CFS
Copper ($\mu\text{g l}^{-1}$)	1.8 to 2.2	1.2 to 1.5	1.3 to 1.3	1.55 ppb
Hardness ($\text{mg-L}^{-1} \text{CaCO}_3$)	49 to 75	52 to 57	60 to 64	59.5 ppm

Little information was obtained regarding Polycyclic Aromatic Hydrocarbon (PAH) levels in Columbia River sediments. Pastorok, *et al.* (1994) found 22 ppm (organic carbon) total PAH at reference sites on the Willamette River near its confluence with the Columbia River. Total Organic Carbon (TOC) represented 1.9% of these sediments. Therefore the reference area PAH concentration was less than 0.418 ppm (dry sediment weight). Sediments at the site were 65% sand and 28% silt, characteristic of low flow areas.

The current analysis assumes that total PAH levels at project sites will be 0.5 ppm (dry sediment weight) and TOC will be assumed to be 1.9%. The Puget Sound Protocols (PSEP, 1986) stipulate that the upper two centimeters of sediment are to be retained for chemical analysis. Therefore, when PAH concentrations are discussed in this report, they are assumed to be based on the concentration in the upper 2 cm of the sediment column.

Toxicity of copper to aquatic fauna and flora with emphasis on salmonids. Brooks (1995b and 1995c) has reviewed available copper toxicity data. Dissolved copper levels as low as 6.1 ppb have been associated with acute toxicity in the most sensitive marine organisms. The sperm of salmon are effected at 44.2 ppb dissolved copper. Coho salmon smolts have an EC₅₀ of 601 ppb copper.

Copper can have more subtle effects on fish. Gardner and LaRoche (1973) reported olfactory damage in mummichogs (*Fundulus heteroclitus*), following even brief encounters (6 hours) with elevated copper levels. Giattina, *et al.* (1982) reported copper avoidance in rainbow trout (*Oncorhynchus mykiss*) at levels of 4.4 - 6.4 ppb in soft water (28 ppm as CaCO₃). However, these same trout were apparently attracted to higher copper levels (334 to 386 ppb). These studies suggest that coho salmon and rainbow trout (two species in the genus *Oncorhynchus*) will avoid areas with copper levels elevated above 4.4 ppb and therefore avoid the stress associated with low levels of copper exposure.

Drummond, *et al.* (1973) observed changes in the feeding behavior of brook trout (*Salvelinus fontinalis*) when exposed to low levels of copper. Feeding was reduced for 24 hours in a constant exposure to 6 ppb copper and for 14 days at 12 ppb. These effects appeared to be transient and McKim and Benoit (1971) reported that normal feeding behavior was resumed within two weeks during a continuous exposure to 9 ppb copper.

Lorz and McPherson (1976) exposed ten to eighteen month old coho salmon (*Oncorhynchus kisutch*) to varying levels of copper and then released them into a tributary and observed migratory behavior. Exposure to 5 ppb copper for 165 days resulted in a 30% reduction in downstream migration. Short term (one to three day) exposure to low levels (<8 ppb copper) were not investigated. However, it appears that copper levels above 5 ppb should be avoided during periods of active salmonid migration. However, based on the work of Giattina, *et al.* (1982), salmonids would be expected to avoid localized areas with copper concentrations exceeding 4.4 ppb.

McKim and Benoit (1971), Gardner and LaRoche (1973) and Scudder, *et al.* (1988) detected a positive copper dose-response effecting hatching time and success in several species of fish. Hazel and Meith (1970) report that copper levels exceeding 100 ppb will kill king salmon (*Oncorhynchus tshawytscha*) eggs. However, no mortality was observed at 8 ppb copper. Other species are more tolerant. Mummichog and silverside fry hatch in ambient levels of up to 5,000 ppb copper (Gardner and LaRoche, 1973).

Reproductive success is negatively influenced by elevated copper levels in numerous species. The available information is reviewed by Sorensen (1991). Scudder, *et al.* (1988) report 17% premature hatching in brook trout eggs incubated at 32.5 ppb copper. No adverse effects were observed at copper levels less than 17.4 ppb copper. Mount and Stephen (1969) report that while copper concentrations of 18.4 ppb kill half of the fathead minnows (*Pimephales promelas*) used in reproductive studies, survival, growth, and reproduction were normal at 4.4 to 10.6 ppb copper. They did observe higher NOEL (No Observed Effects Levels) in hard water (200 ppm CaCO₃).

In summary, fresh-water species of fish are more sensitive to metals than are marine species. Higher salinity and hardness protect fish from copper poisoning as do factors such as pH, dissolved organic material and alkalinity which increase the potential for Cu⁺² complexation and detoxification. It appears that growth and survival are affected at higher copper levels than is successful migratory behavior, reproduction and survival of larval stages. Copper levels greater than 17.4 ppb can adversely effect the number of eggs spawned, hatchability and larval survival. At intermediate hardness values (ca. 50 ppm CaCO₃) migratory impairment can occur at constant copper levels as low as 5 ppb. This suggests that Washington State regulatory levels for copper are adequate to

insure reproductive success with the exception that more strict standards should be imposed (≤ 5.0 ppb) during periods of active salmonid migration.

Summary for copper toxicity Most potentially toxic substances are regulated at the Federal and State Levels. It appears that these regulatory levels are sufficient to protect aquatic species. However, long term exposure to copper levels exceeding 5 ppb should be avoided during the time in which anadromous fish are migrating.

Copper is clearly the metal of most concern in both fresh water and marine environments. From a purely biological point of view, the cupric ion should be maintained below 6 ppb in marine environments. Either the EPA limit of 2.4 ppb (dissolved copper), or the Washington State marine standard of 2.5 ppb appear adequate to protect marine life.

In fresh water, at hardness values of 50 ppm (CaCO_3), the No Observed Effect Level (NOEL) for copper appears to be in excess of 8.0 ppb. Acute effects are observed at significantly higher levels in all fish species studied (50 to 200 ppb). However, reproductive success can be impaired at copper levels as low as 17.4 ppb and migratory behavior (primarily chemoreception) is effected by long term exposure to copper levels greater than 5.0 ppb. Salmonids have been shown to avoid copper concentrations exceeding 4.4 ppb. Therefore, unless the avoidance reaction causes a change in migratory patterns, the Washington State water quality criteria are adequate to protect fresh-water fauna - except during periods of active salmonid migration when total dissolved copper levels should be restricted to 5 ppb.

Water column copper standards. Washington State, in Chapter 173-201A WAC, defines water quality standards for surface waters. The WAC states that toxic substances shall not be introduced above natural background levels in waters of the state which have the potential either singularly or cumulatively to adversely affect characteristic water uses, cause acute or chronic toxicity to the most sensitive biota dependent upon those waters, or adversely affect public health, as determined by the Department of Ecology. Table 2 lists criteria established for the protection of aquatic life in Washington State calculated at 50 ppm hardness (CaCO_3).

Table 2. Water Quality Standards for Surface Waters of the State of Washington. Values are expressed as parts per billion (ppb). A hardness of 50 ppm was used for values requiring computation. See WAC 173-201A-040 for details.

Contaminant	Fresh Acute	Fresh Chronic	Marine Acute	Marine Chronic
Arsenic	360	190	69	36
Chromium (VI)	16.0	11.0	1,100.0	50.0
Copper	8.0	5.6	2.9	-
Zinc	58.0	52.5	84.6	76.6

The Washington State chronic copper standard of 5.6 ppb copper at 50 ppm hardness is slightly higher than the minimum level (5.0 ppb Cu) associated with migratory dysfunction in salmonids. Therefore, it may be appropriate to modify this standard to read, “not to exceed 5.0 ppb copper during the period in which anadromous or catadromous fish are migrating.”

Toxicity of Polycyclic Aromatic Hydrocarbons to aquatic fauna and flora with emphasis on salmonids. Brooks (1995a) has reviewed the available literature regarding PAH toxicity in aquatic environments. The lowest levels of dissolved PAH found to be toxic to aquatic organisms was 8 ppb naphthalene for the larvae of the Dungeness crab (*Cancer magister*) and 18 to 21 ppb for mysids

(*Mysidopsis bahia*). At levels this low, PAH have been found to stimulate plant growth (Boney, 1974 cited in Neff, 1979).

Vertebrates readily metabolize most PAH and elicit acute toxic responses only at very high levels. Borthwick and Patrick (1982) found a 96-h LC₅₀ of 3,500 ppb (unspecified PAH) in Sheepshead minnows (*Cyprinodon variegatus*) and of 150,000 ppb naphthalene in mosquito fish (*Gambusia affinis*).

Pastorok *et al.* (1994) investigated the effects of sedimented PAH associated with a creosote treating plant located on the Willamette River in Oregon. They observed total sedimented PAH as high as 540 ppm (TOC) or 10.26 ppm (dry sediment weight assuming 1.9% TOC). These author's assessed the effects on organisms at this site by conducting Microtox and *Hyalella* bioassays. In addition to sediment chemistry, bioaccumulation studies in fish (*Catostomus macrocheilus*) and crayfish (*Pacifastacus leniusculus*) were complimented with a histopathological survey of the livers of the large-scale sucker (*Castostomus macrocheilus*). The author's conclude that,

“The data on liver histopathology of large-scale sucker collected as part of the remedial investigation and available histopathological data on carp collected at river mile 7 as part of a separate study suggest that risk to fish populations attributable to chronic toxicity from contamination at the site is low. There is no evidence of adverse biological effects throughout most of the main channel of the river. Evaluation of tissue contaminant data for crayfish and large-scale sucker and comparisons of sediment chemistry data for three PAH compounds (acenaphthlene, phenanthrene, and fluoranthene) with available sediment-quality criteria proposed by the U.S. Environmental Protection Agency support this conclusion.”

The literature does not provide clear guidance regarding the levels of sedimented PAH which are injurious to aquatic organisms. Brooks (1995a) reviewed the potential for PAH induced cancer in fish. Included in that review are discussions regarding PAH induced enzyme systems. Taken all together, the literature suggests that PAH metabolizing enzymes are induced at sediment PAH levels between 1.0 and 4.0 ppm (dry sediment weight). There is clear evidence of increased hepatic disease in fish chronically exposed to sediment levels above 25 ppm PAH (dry sediment weight).

It appears that the best currently available guide lies in the Apparent Effects Threshold (AET) based Marine Sediment Quality Standards adopted by Washington State in WAC 173-204-320. Standards have not been adopted for fresh water sediments. This analysis will use the marine standards in the analysis that follows. They are summarized in Table 3.

Table 3. Washington State Apparent Effects Threshold Based Sediment Criteria for Polycyclic Aromatic Hydrocarbons.

Compound Class	Criteria (in ppm TOC)	Criteria at 1.9% TOC (expressed in ppm sediment dry weight)
HPAH	960	18.2 ppm
LPAH	370	7.0 ppm
TOTAL PAH	1,330	25.3 ppm

Modeling sediment concentrations of Polycyclic Aromatic Hydrocarbons in lotic systems. The models presented in Brooks (1995a, 1995b and 1995c) were optimized for poorly circulated marine environments where harmonically driven tidal currents interact with weak steady state currents. The dilution algorithms for these models are modified in the following paragraphs to provide more accurate predictions in lotic systems. This dilution model assumes that water is passing a piling with constant velocity. Turbulence associated with the piling creates the geometry described in Figure 1.

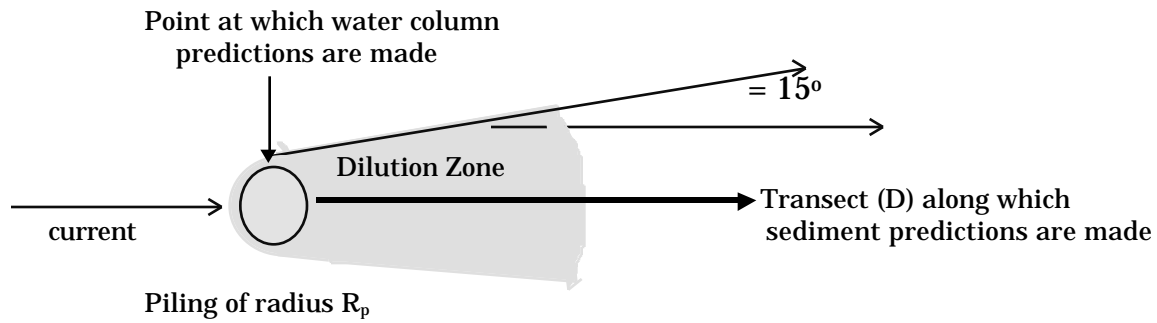


Figure 1. Dilution zone geometry used to predict copper and PAH concentrations in the water column and sediments associated with the use of treated wood.

In this model we let $dA = 2R_p dD + 2D dD$, where

dA = the incremental area

R_p = radius of the piling

dD = the incremental distance along transect D

= the angle representing turbulent mixing = $15^\circ = 0.2618$ radians

Simplifying, we obtain $dA = 2(R_p + 0.2618D)dD$ and let $D = h(V_{ss}/V_v)$

and $dD = (V_{ss}/V_v)dh$, where:

V_{ss} = the steady state current velocity at the site

V_v = the vertical velocity of silt to which the metal or PAH is adsorbed

The expression then becomes $dA = 2(R_p + 0.2618hV_{ss}/V_v)V_{ss}/V_v$

When this is combined with the appropriate expression describing the PAH or copper loss per square centimeter (m) described in Brooks (1995a, 1995b or 1995c), we have an expression for the sediment deposition of copper or PAH.

$$\text{Deposition} = M/dA = 2 R_p m / [2(R_p + 0.2618hV_{ss}/V_v)(V_{ss}/V_v)dh]$$

This expression can be further simplified by substituting $h = DV_v/V_{ss}$ to obtain the final form of the algorithm describing sediment deposition of PAH in $\mu\text{g}\cdot\text{cm}^{-2}\cdot\text{day}^{-1}$.

$$\text{Deposition } (\mu\text{g}\cdot\text{cm}^{-2}\cdot\text{day}^{-1}) = R_p m V_v / [(R_p + 0.2618D)V_{ss}]$$

The sediment accumulation of copper or PAH is predicted by combining this dilution algorithm with the total copper or PAH lost from the piling. Brooks (1995b, 1995c) has shown that copper accumulation in sediments is a very small fraction of

the allowable (WAC 173-205) sediment copper standard in Washington State. Therefore only the results of PAH accumulation in sediments will be discussed here.

$$\text{PAH accumulation} = R_p V_v (24.4 + 0.78T - 0.58S) \exp^{-(\text{age}/10)} \times \exp^{-(\text{actual retention}/22.4 - 1)/2} \\ 0.225 \times 0.047T \exp^{[(4 - \text{RPD})/3]} / [V_{ss}(R_p + 0.2618D)]$$

Modeling water column concentrations of PAH in lotic systems. A conservative model for PAH concentrations in lotic systems assumes that the PAH lost from a piling are diluted in a column of water defined by the current speed and the diameter of the pile. The following equation defines such a dilution zone after converting velocities from centimeters per second to centimeters per day to correspond with the algorithm used to define PAH migration rates.

$$\text{Dilution} = 2R_p V_{ss} 86,400$$

The dilution zone is not a function of the depth of water because we assume that currents are equal at all depths. Therefore the PAH lost from an incremental piling height is diluted in an incrementally high volume of water defined by the piling diameter and steady state current flow. Combining this dilution volume with the predicted PAH migration rate gives a very conservative prediction of the water column concentration of PAH associated with a creosote treated piling:

$$\text{PAH}_{\text{Water Conc.}} = (24.4 + 0.78T - 0.58S) \exp^{-(\text{age}/10)} \times \exp^{-(\text{actual retention}/22.4 - 1)/2} \\ \times 0.225 \times 0.047T \exp^{[(4 - \text{RPD})/3]} / (86400V_{ss})$$

Modeling water column concentrations of copper associated with CCA treated wood in lotic systems. The dilution model for water column concentrations of PAH derived in the preceding section are used to predict water concentrations of copper herein. When combined with the copper loss algorithm provided in Brooks (1995b), we obtain:

$$\text{Copper}_{\text{Water Conc. (CCA)}} = 0.51 \exp^{-0.048 * \text{time (days)} + 0.02 * \text{Salinity (ppt)}} \times (0.55 + 0.65 \ln(0.71 \text{Retention})) \\ / 2R_p V_{ss} 86,400$$

Modeling water column concentrations of copper associated with ACZA treated wood in lotic systems. The dilution model for water column concentrations of copper associated with ACZA treated wood combines the copper loss algorithm developed in Brooks (1995c) and the steady state flow dilution model developed in this report.

$$\text{Copper}_{\text{Water Conc. (ACZA)}} = 1908.6 \exp^{-0.429 \times \text{Days} - 0.383 \times \text{pH}} / 2R_p V_{ss} 86,400$$

Predicted environmental levels of polycyclic aromatic hydrocarbons and copper associated with the use of pressure treated wood piling in lotic systems. Based on the background information presented earlier in this report, the following assumptions were used in making predictions of copper concentrations in receiving waters and PAH accumulation in receiving sediments.

1. Water Temperature = 15°C
2. Salinity = 0.0 ppt
3. Hardness = 59.5 ppm (CaCO₃)
4. Sediment Total Organic Carbon¹ = 1.0 percent
5. CCA and ACZA retention² = 1.0 pcf (15.6 kg-m⁻³)
6. Creosote retention² = 17.0 pcf
7. Background water column copper levels = 1550 ng-L⁻¹
8. Background sediment PAH levels³ = 0.5 µg-g⁻¹

Notes:

¹ The 1.9 percent TOC value reported by Pastorok (1994) for the Willamette River seems high in the author's experience. In this analysis we will assume that sediment TOC is 1.0 percent. While this value would be high in areas of high current, this report will focus on a worst case analysis which involves slow currents, fine sediments and higher levels of TOC. In these areas, a value of 1.0 percent is considered conservative.

²These are the retention's prescribed for fresh water use by AWWA (1992).

³This value is consistent with the report of Pastorok (1994) and with observed background PAH levels in undeveloped areas of Puget Sound. Because of the bedload movement in most areas of the Columbia River, and high sediment deposition, observed values are expected to be lower, except in heavily industrialized areas.

Polycyclic aromatic hydrocarbon predictions and recommendations.





Table 4 provides a summary of maximum predicted PAH accumulation in sediments associated with two creosote treated piling spaced one meter apart. The closest point of approach to the piling computed in these calculations was 5 cm.

This analysis is based on the Washington State Apparent Effects based Marine Sediment Quality Standards. If there is significant documentation demonstrating the need for lower levels, then those levels should be substituted in this analysis as soon as steps are initiated to change the Washington Administrative Code.

Table 4. Predicted maximum PAH concentrations associated with two 30 cm diameter, creosote treated, piling placed one meter apart.

Temp. = 13.3°C, creosote retention = 17 pcf. Current speeds and the depth of the redox potential discontinuity (RPD) are allowed to vary.

Current Speed (cm-sec ⁻¹)			Depth of RPD (cm)			
	0.5	1.0	1.5	2.0	3.0	4.0
0.5	192.19	106.75	70.05	52.8	40.75	39.27
1.0	96.1	53.4	35.0	26.4	20.38	19.6
2.0	48.1	18.3	17.5	13.2	10.2	9.8
3.0	32.0	17.8	11.7	8.8		
4.0	24.0	13.3	8.8			
5.0	19.2	10.7	7.6			
6.0	16.0	8.9	5.8			
7.0	13.7	7.6	5.0			
8.0	12.0	6.7	4.4			
9.0	10.7	5.9	3.9		2.3	2.2
10.0	9.6	5.3	3.5		2.0	2.0
11.0	8.7	4.8	3.2		1.9	1.8
12.0	8.0	4.4	2.9	2.2	1.7	1.6
13.0	7.4	4.1	2.7	2.0	1.6	1.5
14.0	6.9	3.8	2.5	1.9	1.5	1.4
15.0	6.4	3.6	2.3	1.8	1.4	1.3
20.0	4.8	2.7	1.8	1.3	1.0	1.0
25.0	3.8	2.1	1.4	1.1	0.8	0.8
30.0	3.2	1.8	1.2	0.9	0.7	0.6

-  Likely to Effect . Requires a Sediment Impact Zone or Alternate Material
-  Not Likely to Effect. However, project requires an individual assessment
-  Not Likely to Effect. Does not require further assessment.
-  No Effect

The **No Effect level** has been set at sediment PAH levels $\leq 25\%$ of the sediment standard less anticipated background ($0.25 \times 13.3 - 0.5 = 2.3$ ppm TPAH; dry sediment basis).

The **Not Likely to Adversely Effect Level** is set at the Sediment Standard less background and a 25% safety margin ($13.3 \times 0.75 - 0.5 = 9.5$ ppm TPAH; dry sediment basis at 1% TOC) .

Projects for which predicted sediment PAH exceeds the Not Likely to Adversely Effect Level but do not reach the Likely to Adversely Effect Level (12.8 ppm TPAH; dry sediment weight) should be required to conduct an individual risk assessment.

The **Likely to Adversely Effect Level** is highlighted with a dark background. These predictions exceed Washington State Marine Sediment criteria. The Washington State Marine Sediment Standard for 1.0 TOC sediments is 13.3 ppm Total PAH (dry sediment weight). Subtracting the anticipated background (0.5 ppm TPAH; dry sediment weight) indicates that a creosote treated wood project could add 12.8 ppm Total PAH without exceeding the criteria. If predictions suggest that this

level will be exceeded, then alternate materials should be recommended unless the project is of such nature that a Sediment Impact Zone is appropriate.

Creosote Summary. The following generalities can be deduced from Table 4. They provide simple guidelines for permitting creosote treated wood projects:

Recommendation 1. Creosote treated wood projects can be permitted without further risk assessment in the following instances:

- a. when the RPD is ≥ 0.5 cm and current speeds are greater than 10.0 cm/sec
- b. when the RPD is ≥ 1.0 cm and the sum of the RPD (measured in cm) and the current speed (measured in cm-sec⁻¹) exceeds 7.0.

Recommendation 2. An individual project risk assessment should be required in the following circumstances:

- a. when the RPD is < 0.5 cm deep or when current speeds are ≤ 2.0 cm/sec
- b. for projects in which more than four piling are installed in a line parallel to the currents at interpiling distances less than 1.0 meter. This would include dolphins with more than 4 piling. Table 4 was developed using two piling. In the worst case, adding two additional piling in line with the current (spaced one meter apart) would add an additional 3.2 ppm at the downstream piling resulting in a total predicted TPAH accumulation of 13.9 ppm which is just over the Washington State Standard.
- c. when the sum of the RPD and the current speed is ≤ 5.0 .
- d. when a new project is located within 10 meters of an existing creosote treated wood project.

Recommendation 3. Creosote projects shall not be constructed in areas where current speeds are ≤ 1.0 cm-sec⁻¹ without a Sediment Impact Zone authorization.

Copper predictions and recommendations for the use of ACZA treated piling. The following analysis assumes that installation of the project occurs within a single day. Predictions are made at the completion of the project (day 1).

The analysis is based on Washington State water quality criteria published in WAC 173-201. The copper criteria (6.54 ppb) is based on a water hardness of 59.5 ppm CaCO₃ which is the average value reported by Johnson and Hopkins (1991) for the Lower Columbia River. This analysis is appropriate for those periods when salmonids are not actively migrating in the area of the project. An alternate criteria

of 5.0 ppb copper should be imposed on projects constructed within one week of an active salmonid migration.

Background levels are assumed to be 1.55 ppb which is the average reported by Johnson and Hopkins (1991). Thirty centimeter diameter piling, treated to 1.0 pcf (15.6 kg-m⁻³) are assumed to be installed in fresh water with a pH of 8.11. The steady state dilution model developed in this report is used to predict copper concentrations immediately adjacent to the piling. Water column copper concentrations for a variety of current speeds are predicted in Table 5.

Table 5. Water column copper concentrations immediately adjacent to a 30 cm diameter piling, treated with ACZA to a retention of 15.6 kg-m⁻³, as a function of current speed. Ambient pH is 8.11, background copper levels are 1.55 ppb, and the salinity is 0.0 ppt. Washington Standard = 6.540 ppb Cu.

Current Speed (cm-sec ⁻¹)	Total Predicted Copper (ppb)	Copper added by ACZA project (ppb)
0.3	8.291	6.741
0.4		
0.5		4.045
1.0	3.572	2.022
2.0	2.561	1.011
3.0	2.224	0.674
4.0	2.056	0.506
5.0	1.954	0.405
10.0	1.752	0.202
15.0	1.685	0.135

█ Likely to effect for one to two days.

█ Not Likely to Effect

□ No Effect

Based on this analysis, it does not appear that the use of ACZA treated piling presents a threat to aquatic resources when used in open systems with flushing currents ≥ 0.5 cm-sec⁻¹. If ACZA piling are installed in an enclosed area (non flushing), then a minimum surface area of 3,041 square feet is required per piling. That is approximately 14 piling per surface acre. This will maintain water column copper levels at less than Washington State water quality criteria for the conditions described. If more than 14 piling per surface acre are required, then installation should proceed in steps with a maximum of 14 piling installed in any one week period.

It should be emphasized that copper is a natural component of the earth's surface. At an average water column concentration of 1.55 ppb, the Columbia River

carries 4,808 kilograms of copper past an ACZA project every seven days. This is the period in which most of the copper is lost from the piling (see Brooks, 1995b). On the basis of mass loading, an ACZA piling project consisting of 100 piles, standing in 5 meters of water, would contribute an additional 0.893 kilograms of copper. This increases the Columbia River's load by 0.019 percent. Very little metal is lost from ACZA after this initial period. Note that this analysis does not include the Columbia's bed load of copper.

These recommendations protect the migratory fidelity of salmonids. There is an additional safety factor in that olfactory rosette compromise reported by McPherson (1976) occurred following exposure to 5.0 ppb copper for 165 days. Most ACZA metal loss occurs within the first few days following emersion and a return to background levels is anticipated within seven days. In fact, the Washington State chronic copper criteria applied in this analysis is, "A 4-day average concentration not to be exceeded more than once every three years on the average." The four day average copper concentration associated with ACZA treated piling is only 88.7% of the predicted values for day 1. This provides another safety factor in this analysis.

Lastly, reproductive effects in salmonids have not been reported at copper levels less than 17.4 ppb copper. Hazel and Meith (1970) reported that copper levels exceeding 100 ppb will kill king salmon (*Oncorhynchus tshawytscha*) eggs and that no mortality was observed at 8 ppb. All of these effects levels are significantly higher than those predicted for ACZA treated wood at current speeds ≥ 0.4 cm-sec⁻¹.

The previous predictions are based on average hardness and copper background copper levels in the Columbia River. The proposed criteria are also adequate to protect salmonids at the highest ambient copper levels (1.55 ppb) reported by Johnson and Hopkins (1991), and they are within Washington State fresh water quality criteria at the lowest reported hardness level (49 ppm CaCO₃).

ACZA Recommendations. This analysis suggests that the use of ACZA treated wood in the Columbia river presents No Effect to aquatic resources including threatened or endangered species at current speeds greater than 0.5 cm-sec⁻¹. The following should be consider Not Likely to Effect projects for which individual risk assessments are recommended:

1. When greater than 100 piling are to be installed in any one week period.
2. When piling are to be installed in a closed, or very poorly flushed, body of water (current speeds < 0.5 cm-sec) with a density of greater than one piling per 3,041 square feet of surface area.
3. When projects are proposed in close proximity to known sources of copper which result in localized increases in background copper.

Copper predictions and recommendations for the use of CCA treated piling. CCA treated piling is not common on the west coast of the United States because Douglas fir is difficult to treat with CCA. However, CCA is a very common wood preservative in other areas of the country and an analysis of its effects on the Columbia River are included for completeness.

The following analysis assumes that installation of the project occurs within a single day. Predictions are made at the completion of the project (day 1). The analysis is based on Washington State water quality criteria published in WAC 173-201. The copper criteria (6.54 ppb) is based on a water hardness of 59.5 ppm CaCO₃ which is the average value reported by Johnson and Hopkins (1991) for the Lower Columbia River. This analysis is appropriate for those periods when salmonids are not actively migrating in the area of the project. An alternate criteria of 5.0 ppb copper should be imposed on projects constructed within one week of an active salmonid migration.

Background copper levels are assumed to be 1.55 ppb which is the average reported by Johnson and Hopkins (1991). Thirty centimeter diameter southern yellow pine piling, treated to 1.0 pcf (15.6 kg-m⁻³) are assumed to be installed in fresh water with a pH of 8.11.

The steady state dilution model developed in this report is used to predict copper concentrations immediately adjacent to the piling. Water column copper concentrations for a variety of current speeds are predicted in Table 6.

These data indicate that CCA treated piling use in the Columbia River present a No Effect application. If CCA treated piling is used in enclosed waters, a total of 20 square meters of pond surface area is required for each piling. A total of 207 CCA treated piling per acre is required to reach the Washington State water quality criteria of 6.54 ppb copper at 59.5 ppm hardness.

To put the copper losses from CCA in perspective, consider that a project involving 100 CCA treated piling, installed in five meters of water would add 74.9 grams of copper to the Columbia River during the first 30 days when most of the loss occurs. During those 30 days, the Columbia river transports 26,585 kg of copper in the water column. The copper lost from 100 CCA piling during the first 30 days is equal to the natural copper contained in 7.3 seconds of Columbia River flow.

Table 6. Water column copper concentrations of copper immediately adjacent to a 30 cm diameter southern yellow pine piling, treated with CCA to a retention of 15.6 kg-m⁻³, as a function of current speed. Ambient pH is 8.11, background copper levels are 1.55 ppb, and the salinity is 0.0 ppt.

Current Speed (cm-sec ⁻¹)	Total Copper (ppb)	Copper increase associated with CCA treated piling (ppb)
0.1	1.924	0.374
0.5	1.625	0.075
1.0	1.587	0.037
2.0	1.569	0.019

3.0	1.562	0.125
4.0	1.559	0.009
5.0	1.558	0.007
10.0	1.554	0.004
15.0	1.552	0.003

CCA Recommendations. In open lotic systems, CCA treated southern yellow pine piling does not present a risk to aquatic resources and is a No Effect use.

CCA and ACZA treated wood bulkheads. Large surface area projects, such as bulkheads present a greater risk. Models have been developed to assess these risks by Brooks (1995b, 1995c). These models can be used to determine the behavior of CCA and ACZA treated wood in flowing water with the physical and chemical characteristics of the Columbia River. The results of this analysis are presented in Table 7. It is assumed that three days are required to construct the bulkhead. Computations are for day 3.

Table 7. Minimum flow past newly installed CCA and ACZA treated bulkheads required to meet Washington State copper water quality standards in the Columbia River.

Preservative	Minimum Flow to Meet Washington State Water Quality Standards On Day 1
ACZA	18.5 cm sec ⁻¹
CCA	3.5 cm sec ⁻¹

ACZA losses decline rapidly after the wood is placed in the water. CCA losses are initially lower but reductions in loss rates occur more slowly. In Table 8, the models have been used to predict the elapsed time before the water next to a bulkhead project will meet Washington State water quality criteria. Note that a very conservative model is used to define the mixing width along a bulkhead and that typical mixing widths are less than one meter - even at relatively high current speeds.

Table 8. Time required to meet Washington State copper water quality criteria next to newly installed ACZA and CCA treated bulkheads as a function of current speed. These data are relevant to conditions found in the Columbia River.

Current Speed	Time to meet Washington State fresh water copper standards	
	ACZA	CCA
1 cm sec ⁻¹	15 days	52 days
5 cm sec ⁻¹	7 days	meets standard on day one
10 cm sec ⁻¹	3 days	meets standard on day one

Bulkhead Recommendations. When Columbia River flows do not meet the minimum requirements listed in Table 7, an individual risk assessment should be conducted. That risk assessment should include an analysis of the potential movement of salmonids through the area within 30 days following project completion.

When current speeds exceed 3.5 cm-sec⁻¹, the use of CCA treated wood will maintain copper within water quality criteria at all times. Higher current speeds are required to meet copper criteria on day 1 when ACZA treated wood is used (18.5 cm - sec⁻¹).

Summary and Conclusions. A broad range of conditions has been addressed in this analysis. Creosote use is dictated by currents and the availability of oxygen in sediments. However, there is a significant range of projects and environments where creosote can be considered to have No Effect on aquatic organisms. Care should be exercised in the use of creosote where sediments have low oxygen tensions.

The waterborne treatments (ACZA and CCA) release copper at low levels. In flowing water, the use of piling presents minimal risk to aquatic organisms and the total copper released by piling is a tiny fraction of the natural copper load in the Columbia. In most uses, CCA and ACZA piling should be considered No Effect. In very poorly circulated or closed bodies of water, copper can accumulate in the water column to levels exceeding the Washington State copper criteria and individual risk assessments should be required when surface area requirements are not met.

Large surface area structures (such as bulkheads) can contribute a significant amount of copper over a relatively short period of time. Rather restrictive criteria are proposed to insure the integrity of aquatic resources. When the minimum flow criteria presented in Table 7 are not met, I recommend an individual risk assessment.

Proper Fixation. The metal loss rates used in the analysis were developed from testing of properly fixed CCA and ACZA treated wood. The data was presented as part of the EPA registration of these preservatives and is of very high quality. It should be emphasized that high environmental performance is dependent on proper fixation of the chemicals which is time and temperature dependent. The Western Wood Preservers Institute and the Canadian Institute of Treated Wood have

developed best management practices (BMPs) for the production of treated wood products used in aquatic environments. It is recommended that all permits allowing treated wood use in aquatic environments be conditioned to require production in accordance with these BMP's.

The data used to develop PAH migration rates from creosote treated wood is based on conventionally treated products. It is anticipated that creosote BMP's will significantly improve the environmental performance of creosote treated piling. Creosote treated wood projects should also be conditioned to require production using BMP's.

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